## Digital Resonators

"Discrete-Time Oscillator Theory"
Clay S. Turner

## Discrete-Time Sinusoidal Resonators

- DTSRs may be represented with 2 by 2 real valued matrices.
- DTSRs are easily analyzed using matrix theory.
- DTSRs are compactly represented by matrices.
- DTSR properties are easily gleaned from the matrix representations.
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## Trigonometric Recursion

- Early example from Francois Vieta (1572). Vieta used this formula to recursively generate trig tables.
$\cos (p+q)=2 \cos (p) \cdot \cos (q)-\cos (p-q)$
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## Trigonometric Recursion

- Vieta's formula allow's one to recursively find subsequent values of $\cos ()$ and $\sin ()$ just by using the last two values and a multiplicative factor. E.g.,

$$
\text { Next }=2 \cos (p) \cdot \text { Current }- \text { Last }
$$

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## Network to Matrix Formulation

- Network form of Vieta's recursion (Biquad).
- Biquad has two state variables (memory elements)
- Biquad uses one multiply and one subtract per iteration
- Biquad is most well known sinusoidal recursion.

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## Network to Matrix Formulation



- Label inputs and the outputs of each memory element in the network.
- Then write each input's equation in terms of all outputs.
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## Biquad Iteration Equations


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## Biquad Matrix Formulation

- Matrix Formulation of Vieta's Recursion

$$
\left[\begin{array}{l}
\hat{a} \\
\hat{b}
\end{array}\right]=\left[\begin{array}{cc}
2 \cos (\theta) & -1 \\
1 & 0
\end{array}\right] \cdot\left[\begin{array}{l}
a \\
b
\end{array}\right]
$$

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## Another Trigonometric Example

- Example with two coupled equations
$\cos (p+q)=\cos (p) \cdot \cos (q)-\sin (p) \cdot \sin (q)$
$\sin (p+q)=\sin (p) \cdot \cos (q)+\cos (p) \cdot \sin (q)$
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## Coupled Recursion

- Here we update both $\sin ()$ and $\cos ()$ just using last two values and two multiplies per iteration.

$$
\begin{aligned}
& \text { NxtCos }=\text { CrntCos } \cdot \cos (q)-\text { CrntSin } \cdot \sin (q) \\
& N x t S i n=\text { CrntSin } \cdot \cos (q)+\text { CrntCos } \cdot \sin (q)
\end{aligned}
$$

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## Coupled Iteration Equations

- Just like with the biquad structure, we may write the iteration equations in a similar manner.
- The step angle per iteration is $\theta$

$$
\begin{aligned}
& \hat{a}=a \cdot \cos (\theta)-b \cdot \sin (\theta) \\
& \hat{b}=b \cdot \cos (\theta)+a \cdot \sin (\theta)
\end{aligned}
$$

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## Coupled Matrix Formulation

- Recognized as standard rotation matrix

$$
\left[\begin{array}{l}
\hat{a} \\
\hat{b}
\end{array}\right]=\left[\begin{array}{cc}
\cos (\theta) & -\sin (\theta) \\
\sin (\theta) & \cos (\theta)
\end{array}\right] \cdot\left[\begin{array}{l}
a \\
b
\end{array}\right]
$$

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## Discrete-Time Oscillator Structure

- The two example oscillators have the following in common:
- Each uses 2 state variables.
- The matrix in each case is 2 by 2 .
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## Discrete-Time Linear Oscillators

- So we will look at the following types of oscillator iterations (based on a general 2 by 2 matrix) more closely:

$$
\left[\begin{array}{l}
\hat{a} \\
\hat{b}
\end{array}\right]=\left[\begin{array}{ll}
\alpha_{11} & \alpha_{12} \\
\alpha_{21} & \alpha_{22}
\end{array}\right] \cdot\left[\begin{array}{l}
a \\
b
\end{array}\right]
$$

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## Discrete-Time Barkhausen Criteria

- From the point of view of repeated iteration we see the nth output of the oscillator is simply:

$$
\left[\begin{array}{l}
\hat{a} \\
\hat{b}
\end{array}\right]_{n}=\left[\begin{array}{ll}
\alpha_{11} & \alpha_{12} \\
\alpha_{21} & \alpha_{22}
\end{array}\right]^{n} \cdot\left[\begin{array}{l}
a \\
b
\end{array}\right]_{0}
$$

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## Resonator Theory

- Besides looking at known trigonometric relations, how do we find new oscillator structures?
- Answer: We develop our own theory with guidance from analog theory.
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## Barkhausen's Linear Oscillator Theory

- Heinrich Barkhausen modeled a linear oscillator as a linear amplifier with its output fed back in to its input and then stated two necessary criteria for oscillation.


## Barkhausen Criteria

1. The amplifier gain times the feed back gain needs to equal unity.
2. The round trip delay needs to be a integral multiple of the oscillation period.
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## Discrete Time Osc. Theory

- So combining the matrix representation idea from our two examples with Barkhausen's oscillator theory, we can come up with the discrete time counterparts to the Barkhausen Criteria.


## Discrete Time Barkhausen Criteria

- The determinant of the oscillator matrix must be unity.
- The oscillator matrix when raised to some real power will be the identity matrix.
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## Discrete-Time Barkhausen Criteria

- Thus our two criteria in mathematical terms of matrix A are:

$$
\begin{aligned}
& \operatorname{Det}(A)=1 \\
& A^{\text {period }}=I
\end{aligned}
$$

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## Barkhausen's $1^{\text {st }}$ Criterion

- If we think of the two state variables as components of a vector, then Barkhausen's $1^{\text {st }}$ Criterion relates to length preservation. I.e., this says the length of the vector is unchanged by rotation.


## Barkhausen's $2^{\text {nd }}$ criterion

- The periodicity constraint in combination with the unity gain means the oscillator matrix has complex valued eigenvalues.
- This in turn means the matrix's "trace" has a magnitude of less than 2.


## Discrete-Time Barkhausen Criteria

- Thus our two criteria may alternatively be stated in terms of the actual matrix elements:

$$
\begin{gathered}
\alpha_{11} \alpha_{22}-\alpha_{12} \alpha_{21}=1 \\
\left|\alpha_{11}+\alpha_{22}\right|<2
\end{gathered}
$$

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## Eigen-Theory

- A big advantage of using a matrix representation of the oscillator structure, is we can apply Linear Algebra with its tools to analyze oscillators.
- Eigentheory actually allows us to factor the matrix into a triple product where the step angle and the relative phases are readily apparent.


## Oscillator Eigenvalues

- The oscillator matrix will have two eigenvalues that reside on the unit circle, and they are complex conjugates of each other.
- The eigenvalues are found to be:

$$
\lambda=e^{ \pm j \theta} \quad \text { where } \quad \theta=\cos ^{-1}\left(\frac{\alpha_{11}+\alpha_{22}}{2}\right)
$$

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## Oscillator Step Angle

- The angle theta is the step angle per iteration of the oscillator.
- Thus the oscillator frequency is determined wholly by the trace (delta) of the matrix!


## $\Delta=2 \cos (\theta)$

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## Analysis of the off Diagonal Matrix Elements

- A study of the eigen values along with Barkhausen's criteria will show that the "off diagonal" matrix elements must obey the following:

$$
\alpha_{12} \alpha_{21}<0
$$

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## Properties of the off Diagonal Matrix Elements

- Thus we see that neither off diagonal element may be zero!
- No oscillator matrix may be triangular.
- And we see that they must have opposite signs!


## State Variables

- If the state variables are plotted as a function of time, they will each be a sinusoid, both with the same frequency, be out of phase and may have a relative amplitude not equal to one.
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## Relative Phase shift

- From a study of the eigenvectors, the relative phase shift between the state variables (b relative to a) is:

$$
\phi=\arg \left(\frac{\alpha_{22}-\alpha_{11}+j \sqrt{4-\left(\alpha_{11}+\alpha_{22}\right)^{2}}}{2 \alpha_{12}}\right)
$$

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## Relative Phase Shift (alternative)

- An alternative formulation for relative phase shift is:

$$
\phi=\cos ^{-1}\left(\frac{\alpha_{22}-\alpha_{11}}{2 \sqrt{-\alpha_{12} \alpha_{21}}}\right)+\frac{\pi}{2}\left(\operatorname{sgn}\left(\alpha_{12}\right)-1\right)
$$

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## Quadrature Criterion

- From the phase shift formula, we find that a relative phase of +-90 degrees requires the two elements making up the trace of the matrix to have the same value!
- Thus, from simply looking at an oscillator matrix we can ascertain if the oscillator is quadrature or not.


## Relative Amplitude

- The relative amplitude ( $b$ to $a$ ) is given by:

$$
\psi=\sqrt{\frac{-\alpha_{21}}{\alpha_{12}}}
$$

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## Relative Amplitude

- From our earlier work on the off diagonal elements, we know that the relative amplitude will always be a positive value.
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## Equi-Amplitude Criterion

- The relative amplitude relation tells us that if we are to have both state variables have the same amplitude, then we simply require:

$$
\alpha_{12}=-\alpha_{21}
$$

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## Matrix Factoring

- The main point of the eigenanalysis is to factor the matrix. We find:
$A=\left[\begin{array}{cc}1 & 1 \\ \psi e^{j \phi} & \psi e^{-j \phi}\end{array}\right] \cdot\left[\begin{array}{cc}e^{j \theta} & 0 \\ 0 & e^{-j \theta}\end{array}\right] \cdot\left[\begin{array}{cc}1 & 1 \\ \psi e^{j \phi} & \psi e^{-j \phi}\end{array}\right]^{-1}$
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## Matrix Exponentiation

- The factoring makes raising the matrix to a power straight forward and reveals the nature of theta.

$$
A^{n}=\left[\begin{array}{cc}
1 & 1 \\
\psi e^{j \phi} & \psi e^{-j \phi}
\end{array}\right] \cdot\left[\begin{array}{cc}
e^{j n \theta} & 0 \\
0 & e^{-j n \theta}
\end{array}\right] \cdot\left[\begin{array}{cc}
1 & 1 \\
\psi e^{j \phi} & \psi e^{-j \phi}
\end{array}\right]^{-1}
$$

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## Initialization

- Assuming we have a chosen oscillator matrix, then from eigen-theory, we find the state variables need to be initialized to

$$
\left[\begin{array}{l}
a \\
b
\end{array}\right]=\left[\begin{array}{c}
1 \\
\psi \cos (\phi)
\end{array}\right]
$$

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## Nth output of oscillator

- From eigen-theory, we find the nth output (assuming the aforementioned initialization) to be:

$$
\left[\begin{array}{l}
a \\
b
\end{array}\right]_{n}=\left[\begin{array}{c}
\cos (n \theta) \\
\psi \cos (n \theta+\phi)
\end{array}\right]
$$

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## Oscillator Amplitude

- The amplitude squared (energy) of the oscillator is given by:

$$
E=\frac{a^{2}+\left(\frac{b}{\psi}\right)^{2}-2 \frac{a \cdot b \cdot \cos (\phi)}{\psi}}{\sin ^{2}(\phi)}
$$

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## Amplitude Control

- To keep magnitude errors from growing, a simple "AGC" type of feedback may be employed. Thus a gain " $G$ " is calculated every so often based on the energy, E, and is used to scale the state variables.
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## Useful Amplitude Control

- A $1^{\text {st }}$ order Taylor's series expansion around the desired amplitude square works quite well. Two examples are:

$$
\begin{array}{ll}
G=\frac{3}{2}-E & E_{0}=\frac{1}{2} \\
G=\frac{3-E}{2} & E_{0}=1
\end{array}
$$

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## Digital Waveguide Osc.

- Single Multiply, Quadrature Oscilator

$$
A=\left[\begin{array}{cc}
k & k-1 \\
k+1 & k
\end{array}\right]
$$

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## Dual Multiply - Quadrature

- This oscillator uses 2 multiplies per iteration, has quadrature outputs and uses staggered updating.

$$
A=\left[\begin{array}{cc}
k & 1-k^{2} \\
-1 & k
\end{array}\right]
$$

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## Staggered Updating

- The matrix formulation's compactness is nice, but it implies a simultaneous updating of the state variables.
- Sequential updating may require temporary storage.


## Staggered Updating

- Staggered updating is a method where one state variable is $1^{\text {st }}$ updated and then that updated value is used in the $2^{\text {nd }}$ update equation.
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## Staggered Update - Derivation

- We will start with a pair of staggered updated equations and force Barkhausen's criteria upon them.

$$
\begin{aligned}
& \hat{b}=\alpha \cdot a+\beta \cdot b \\
& \hat{a}=\gamma \cdot a+\delta \cdot \hat{b}
\end{aligned}
$$

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## Staggered Update - Derivation

- So now we insert the $1^{\text {st }}$ update into the $2^{\text {nd }}$ equation and we get the following matrix form:

$$
A=\left[\begin{array}{cc}
\gamma+\alpha \delta & \beta \delta \\
\alpha & \beta
\end{array}\right]
$$

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## Staggered Update - Derivation

- Next we apply Barkhausen's $1^{\text {st }}$ criterion and we find the following 3 parameter matrix

$$
A=\left[\begin{array}{cc}
\frac{1}{\beta}+\alpha \delta & \beta \delta \\
\alpha & \beta
\end{array}\right]
$$

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## EquiAmp-Staggered Update

- To be equi-amplitude, we just set the offdiagonal elements to be negatives of each other.

$$
\alpha=-\beta \delta
$$

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## EquiAmp-Staggered Update

- Thus our 2 parameter equi-amplitude staggered update oscillator has the following form.

$$
A=\left[\begin{array}{cc}
\frac{1}{\beta}-\beta \delta^{2} & \beta \delta \\
-\beta \delta & \beta
\end{array}\right]
$$

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## EquiAmp-Staggered Update

- Now we can substitute some simple values for the parameters and get a couple of neat oscillators.
- First we will set:

$$
\beta=1
$$

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## Magic Circle Algorithm

- The "magically" wonderful oscillator results:

$$
\left[\begin{array}{cc}
1-\delta^{2} & \delta \\
-\delta & 1
\end{array}\right]
$$

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## Magic Circle Algorithm

- The Magic Circle Algorithm's update equations are the simple:

$$
\begin{aligned}
& \hat{b}=b-\delta \cdot a \\
& \hat{a}=a+\delta \cdot \hat{b}
\end{aligned}
$$

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## Staggered Update Biquad

- Another choice for the parameters results in a Biquad oscillator with staggered updating. The tradeoff here is between an extra multiply verses a storage location. To obtain this form just let:

$$
\beta \delta=1
$$

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## Staggered Update Biquad

- The Staggered update biquad's matrix form is:

$$
A=\left[\begin{array}{cc}
0 & 1 \\
-1 & \beta
\end{array}\right]
$$

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## Staggered Update Biquad

- The update equations are:

$$
\begin{gathered}
\hat{b}=\beta \cdot b-a \\
\hat{a}=\frac{1}{\beta} \cdot(\hat{b}+a)
\end{gathered}
$$

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## Reinsch (Staggered Update)

- If we relax the equiamplitude requirement and set 2 of the 3 parameters to unity, then we can obtain Reinsch's formulation. For example:

$$
\beta=1 \quad \delta=1
$$

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## Reinsch (Staggered Update)

- Here we get a the following matrix and corresponding update equations:

$$
A=\left[\begin{array}{cc}
1+\alpha & 1 \\
\alpha & 1
\end{array}\right] \quad \begin{gathered}
\hat{b}=\alpha \cdot a+b \\
\hat{\alpha}=a+\hat{b}
\end{gathered}
$$

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## An Oscillator Application

- The venerable Goertzel Algorithm uses a Biquad oscillator for its calculation.
- However any oscillator may be used in the Goertzel Algorithm.
- Some oscillators will have better numerical properties than others. I.e., especially for low frequencies.


## The Generalized Goertzel Algorithm

- Goertzel processes N values of data and computes a Fourier Coefficient (single frequency) for the data. We can describe this algorithm in four (five) main steps.
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## The Generalized Goertzel Algorithm (Step 1)

- Initialization - uses 1 datum.

$$
\vec{y}_{0}=\left[\begin{array}{c}
x_{0} \\
0
\end{array}\right]
$$

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## The Generalized Goertzel Algorithm (Step 2)

- Recursive computation with all input data. "A" is the oscillator matrix. For

$$
i \in\{1,2,3, \ldots, N-1\}, \vec{y}_{i}=A \cdot \vec{y}_{i-1}+\left[\begin{array}{c}
x_{i} \\
0
\end{array}\right]
$$

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## The Generalized Goertzel Algorithm (Step 3)

- Phase Compensation

$$
\vec{y}_{N}=A \cdot \vec{y}_{N-1}
$$

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## The Generalized Goertzel Algorithm (Step 4)

- Calculation of the Fourier Coefficient

$$
\left[\begin{array}{c}
c_{k} \\
s_{k}
\end{array}\right]=\left[\begin{array}{cc}
1 & -\frac{\cos (\phi)}{\psi} \\
0 & \frac{\sin (\phi)}{\psi}
\end{array}\right] \cdot\left[\vec{y}_{N}\right]
$$

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## The Generalized Goertzel Algorithm (Step 5a)

- Energy Calculation assuming steps 3 and 4 are performed.

$$
E=c_{k}^{2}+s_{k}^{2}
$$

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## The Generalized Goertzel Algorithm (Step 5b)

- If the energy (amplitude squared) is all that is needed, then just skip steps 3 and 4 and calculate the following: ( $a$ and b) are the 2 elements of the last result from step 2.

$$
E=a^{2}+\left(\frac{b}{\psi}\right)^{2}-2 a b \frac{\cos (\phi)}{\psi}
$$

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## Improving Goertzel

- Some choices of oscillator design will yield better numerical accuracy than others.
- For comparison, we show the Biquad, Reinsch, and Magic Circle Oscillators and how they perform in Goertzel.
- For this test. $\mathrm{N}=1000$ points


## Extended Goertzel Results

Rel Err vs Freq.


## Zoomed In View (Results)

Rel Err Vs Freq.

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## Results Explaination

- In low frequency limit:
- Biquad is in phase and equiamplitude
- Reinsch is in phase and amplitudes are unmatched
- Magic Circle is quadrature and equiamplitude.
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## Discrete Time Oscillators

- Thanks to all who are willing to listen ;-)
- The End for Now!
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